



Performance evaluation of hydraulic ram by varying the weight and stroke length of waste valve

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Abstract: A hydraulic ram (50 mm x 25 mm) was designed, fabricated and installed using locally available pipes and fittings and with some components which could be easily made. Test was conducted by varying the stroke length and weight of waste valve. The study revealed that the efficiency of hydraulic ram increased with decrease in stroke length of waste valve. It was also found that there is a minimum weight of waste valve corresponding to a certain weight of delivery valve, at which the hydraulic ram functions satisfactorily. The operating range of hydraulic ram was found to decrease with decrease in the weight of waste valve.

Key Words: Hydraulic ram, Stroke length, Waste valve.

Introduction

In a developing country like India, the difficulties in conveying electrical energy to remote hilly areas and shortage of petroleum fuels have focused the importance of hydraulic ram for lift irrigation and rural water supply. In mountainous regions of India, there are numerous sites where hydraulic rams could be installed, thus reducing the human drudgery in carrying lead loads of drinking water along steep hills and improve the economic conditions of villages through irrigation of dry uplands.

Hydraulic ram runs itself, it needs no external instigating energy source, it is automatic, pollution free, simple in construction, continuous in operation, requires no lubrication and supervision, needs less maintenance and wear is minimum. Despite of these merits, they have not been used widely for irrigation because in the past no serious attempt had been made to popularise the ram (Raveendra and Sheshadri, 1981). Recently, in the wake of power crisis, many of the developed and developing countries are giving more importance in popularising the hydraulic ram. Only few studies have been conducted to optimise various parameters of hydraulic ram. In this study, an attempt is made to fabricate a cheap and economic model of hydraulic ram by using locally available materials and also to study the performance of ram by varying the weight and stroke length of waste valve.

Materials and Methods

The study was conducted at Kelappagi College of Agricultural Engineering and Technology, Tavanur, Kerala. A centrifugal pump was utilised to supply water from a sump to the supply tank of hydraulic ram. During the study, a constant supply head of 1.955 m was maintained. G.I.Pipes having diameter of 50 mm and 25 mm were used as supply and delivery pipes. One end of the supply pipe was connected to the supply tank and the other end to the waste valve. The delivery pipe was connected to the air chamber. A 75 mm diameter GI pipe was used as air chamber. A gate valve was provided in the delivery pipe to control the discharge. The corresponding delivery head was measured using pressure gauge fitted on the delivery pipe. Keeping the delivery head (H_d) constant, the volume of water flowing through the gate valve on the delivery discharge and waste discharge were found out by using the following formula,

$$\text{Delivery discharge } (Q_d) = \frac{V_d}{t} \text{ where,}$$

V_d is the volume of water flowing out through the gate valve on the delivery pipe for a duration of time 't'

$$\text{Waste discharge } (Q_w) = \frac{V_w}{t} \text{ where,}$$

Table 1. Minimum delivery head at which the ram functions

Weight of waste valve (g)	Stroke length of waste valve (mm)	Stroke length of delivery valve (mm)	Minimum delivery head at which ram functions (m)			
			Delivery valve weights (g)			
			185.37	285.37	385.37	485.37
400	42	20	6.25	8.75	*	*
		35	5.25	8.75	*	*
		50	4	9	*	*
400	30	20	5	9	*	*
		35	6	10.75	*	*
		50	5.5	11.5	*	*
400	20	20	5.75	10	*	*
		35	4.5	11	11.9**	12.75**
		50	4.5	11	12.5**	13.5**
500	42	20	4.5	6	12	14.5
		35	4.5	5.5	11.5	14
		50	4	5.5	11	13.5
500	30	20	5	6	14	14.25
		35	4.5	5	12	14
		50	4	4.75	10	13.75
500	20	20	5	7.75	10.5	12.25
		35	4	7	10.8	12.5
		50	3	5	8.5	12
600	42	20	5.5	7	10	12.75
		35	5	5.75	9.8	12.5
		50	4	4.75	8.5	12.25
600	30	20	4	5	9.5	12
		35	4	5	8	11
		50	4	5	8	11
600	20	20	5	6	10.8	14.5
		35	4	6	10.5	14.25
		50	3	4	10	12

* Hydraulic ram did not work

** Hydraulic ram worked for a while, then stopped

V_w is the volume of water flowing through the waste valve for a duration of time 't'.

The general layout of experimental setup is presented schematically in Fig.1 and sectional view of waste valve is given in Fig.2. Provisions were given to change the weight and stroke length of waste valve. In order to study the effect of stroke length of waste valve, three stroke lengths 42 mm, 30 mm and 20 mm were used. Totally three waste valve weights

namely 400 g, 500 g and 600 g were used in the present study.

In each set up of the instrument, performance of hydraulic ram was evaluated mainly observing delivery head-delivery discharge relationships. In each case the efficiency (η) was also calculated using the D' Aubuisson's efficiency formula,

$$\text{D' Aubuisson's efficiency } (\eta) = \frac{Q_d H_d}{Q_s H_s} \text{ where,}$$

supply discharge (Q_s) = $Q_d + Q_w$ and supply head (H_s) = 1.995 m

Results and Discussion

In order to study the effect of stroke length of waste valve, observations were taken by keeping other parameters namely weight of waste valve, weight and stroke length of delivery valve and volume air chamber constant. Curves showing the variation of delivery discharge with delivery head for different stroke lengths of waste valve are given in Fig (3) and Fig (4). The curves showed that there was substantial decrease in delivery discharge with slight increase in the delivery head. It was also seen that the delivery discharge corresponding to a given value of delivery head, increased with decrease in stroke length of waste valve, when all other parameters were kept constant. The possible explanation for this is that with the reduction of stroke length, number of strokes per minute gets increased. The time during which the waste valve remained open decreased with decrease in stroke length of waste valve, which reduced the wastewater per each cycle of operation. Moreover, the number of times the water forced into the air chamber increased and hence the delivery discharge increased. The curves showing the relation between delivery head and efficiency (Fig.3) revealed that efficiency increased with increase in delivery discharge upto a certain point and after that efficiency decreased slowly with increase of delivery head. It can also be seen that the delivery head corresponding to maximum efficiency for different stroke lengths of waste valve was more or less the same.

At higher delivery head, the time during which the waste valve off its seat increases and hence the waste discharge increases (Gibson, 1930). The increased wastage will decrease the efficiency. At one stage, when delivery head further increases, the increase in gain due to increase of delivery head is less than the loss due to increase in wastage resulting, a lower efficiency. Also the shock and frictional losses in the supply and delivery pipes increase with increase in the delivery head. Further, loss of energy due to resilience is proportional to the square of delivery head. At higher delivery head, these losses will be large and hence efficiency gets reduced. Hence efficiency of ram was

found to be maximum at moderate delivery head. However in the case of lighter waste valve, the efficiency was continued to decrease with increase in delivery head (Fig.4) upto a certain point and after that ram stopped functioning. For lower weight of waste valve, hydraulic ram stopped functioning comparatively at higher delivery head (i.e. at lower delivery discharge) and operating range of hydraulic ram was found to decrease with decrease in the weight of waste valve. Moreover, for lower weight of waste valve, as stroke length of waste valve decreases, ram was found to operate comparatively in high range of delivery heads. But for a heavier waste valve, hydraulic ram operated even for higher delivery discharge though the corresponding delivery head was small. So to have a large delivery discharge, we must use a heavier waste valve (when all other parameters are constant). The possible explanation for the stoppage of operation of the ram at lower delivery head is at lower delivery heads, the pressure developed in the air chamber will be less than the pressure generated under conditions of higher delivery heads. This means that under lower delivery heads, the delivery valve will open under relatively lower pressure.

The positive water hammer pressure generated by the sudden closure of waste valve will obtain a relief before it attains its maximum value. Magnitude of the consequent negative pressure developed will also be less. Negative pressure developed under low head conditions will not be sufficient to open the waste valve and ram will not work on its own. Under higher delivery head conditions, delivery valve opens after the positive water hammer pressure attains higher value. The consequent negative pressure developed will also be high. This will be sufficient to open the waste valve and the ram will work on its own repeating the cycle. Thus, for the same weight of delivery valve, when the weight of waste valve was increased, the negative pressure developed might be sufficient to open the heavier waste valve and hence the ram functioned smoothly even at lower delivery head and higher delivery discharge. It was also seen that efficiency increased as the stroke length decreased. This may be mainly due to the fact that as the stroke length decreases

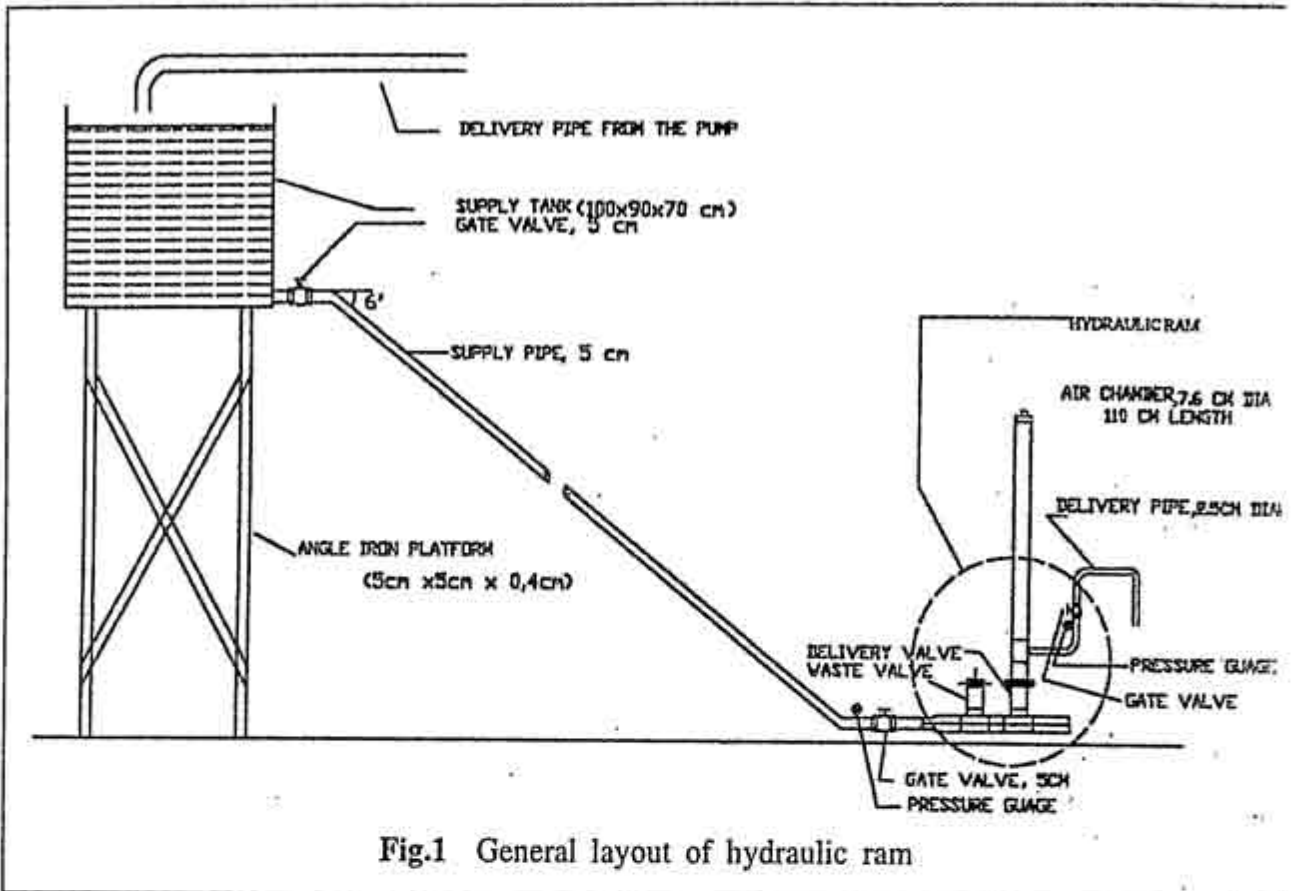


Fig.1 General layout of hydraulic ram

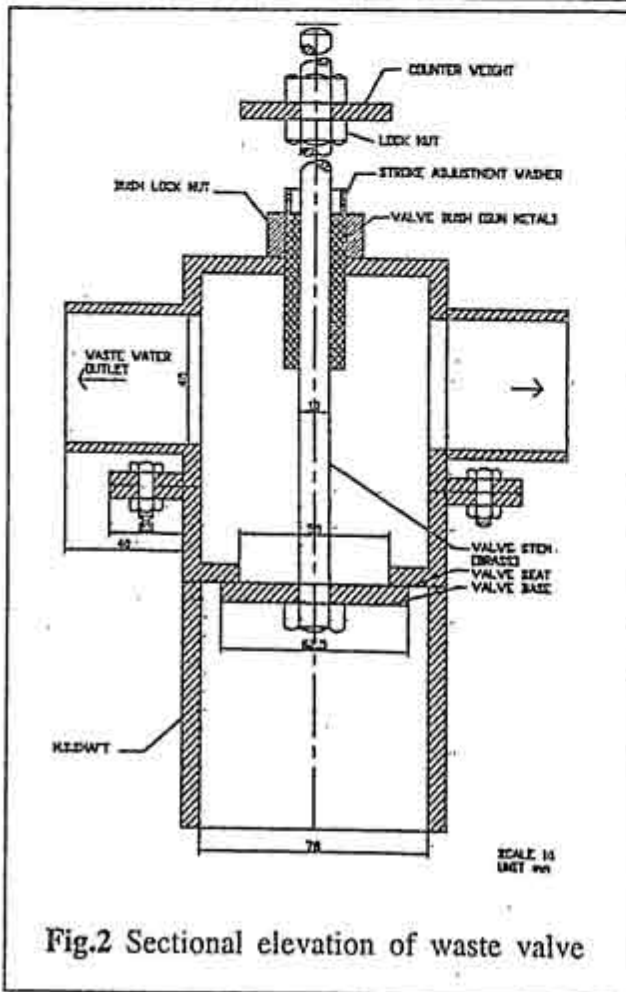


Fig.2 Sectional elevation of waste valve

number of times water forced into the air chamber for a unit period of time increase and for a particular volume of water washed through waste valve, the delivery discharge gets increased.

From the above discussion, it can be seen that the delivery head of the ram is an important parameter affecting the efficiency. Calvert (1958) found that the ratio (H_d/H_s) is the most influencing dimensionless parameter on the performance of the ram. But in this study, supply head was constant and so head ratio is only a function of delivery head. It was found that the results obtained in the study are also consistent with the findings of Calvert on the same aspect.

From the Table 1 it is clear that weight of the waste valve had also significant effect on the performance of ram. When the weight of delivery valve was increased from 285.87 g to 387.37g, hydraulic ram was not working smoothly with the waste valve having a weight of 400 g. By increasing the weight of waste valve to 500 g, the hydraulic ram worked

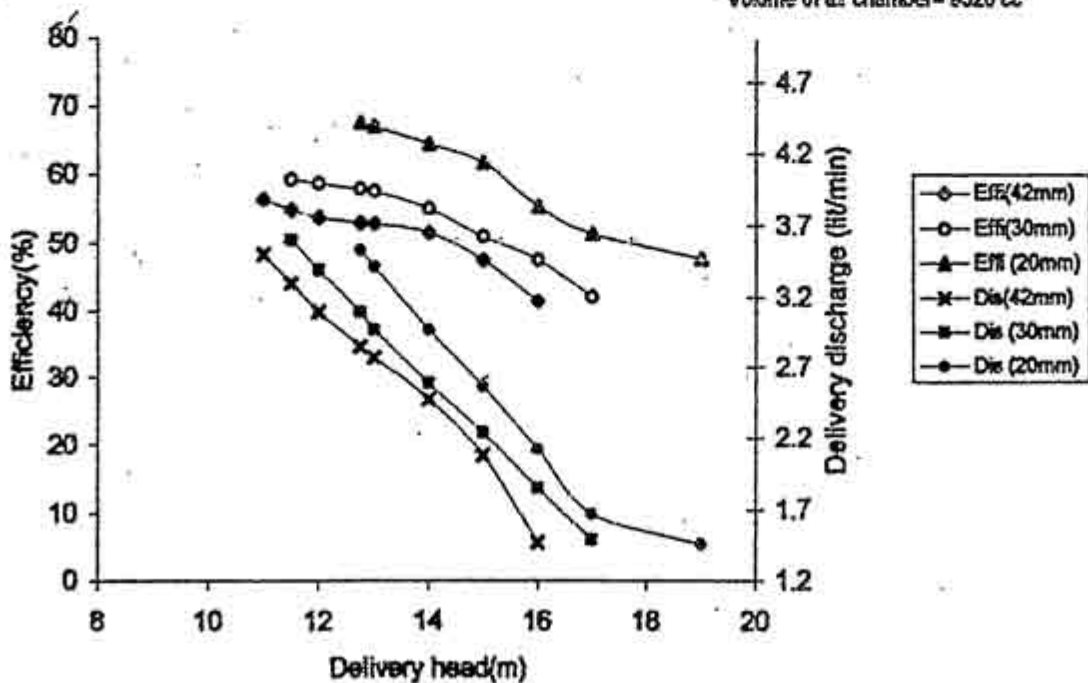
Fig.3 Effect of stroke length of waste valve on the performance of hydraulic ram

Wt. of waste valve = 600g
 Wt. of delivery valve = 285.37g
 stroke length of delivery valve = 50mm
 Volume of air chamber = 9520 cc



Fig.4 Effect of stroke length of waste valve on the performance of hydraulic ram

Wt. of waste valve = 400g
 Wt. of delivery valve = 285.37g
 Stroke length of delivery valve = 50mm
 Volume of air chamber = 9520 cc



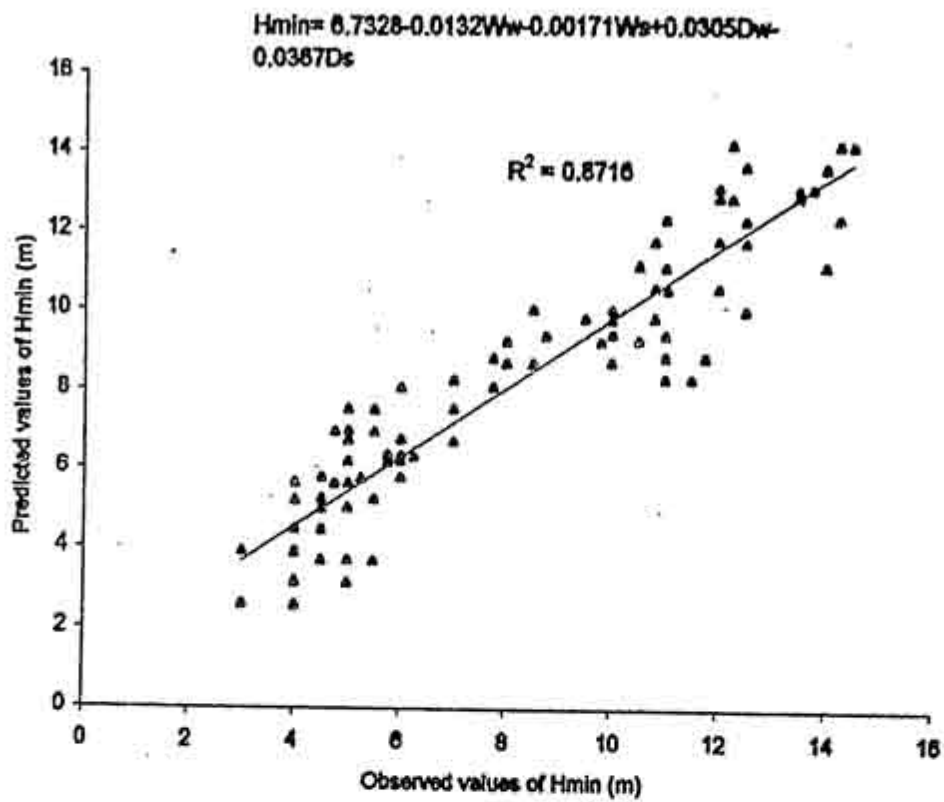


Fig.5 Observed versus predicted values of minimum delivery head

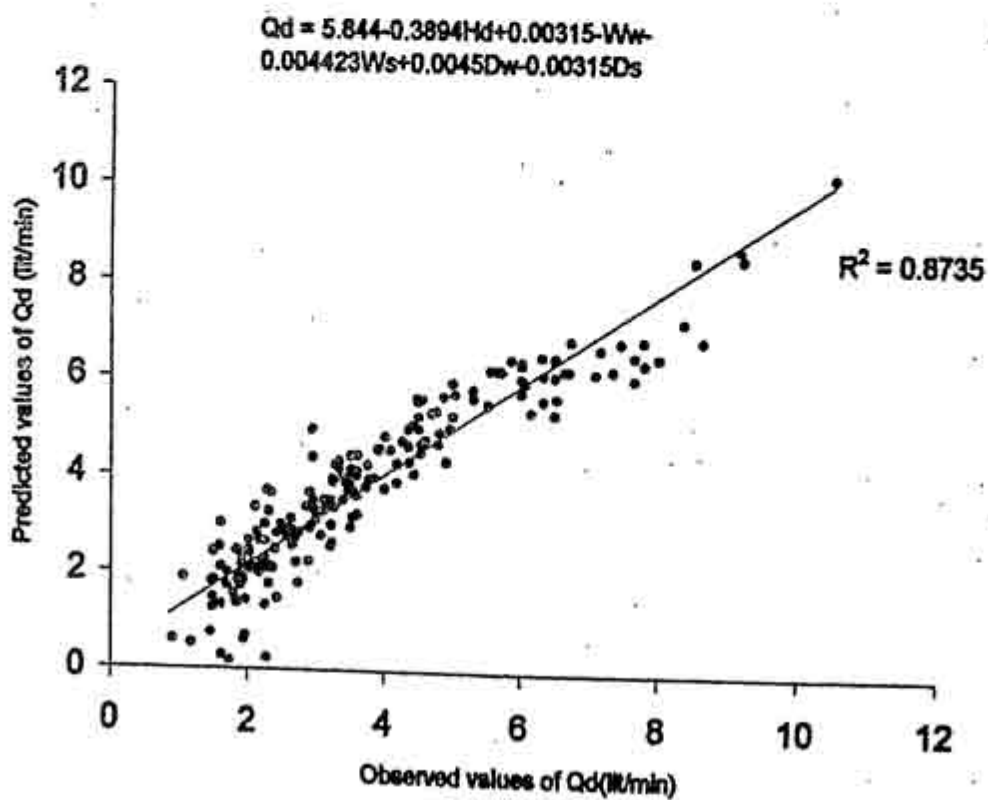


Fig.6 Observed versus predicted values of delivery discharge

smoothly even with the heavier delivery valve. The result indicates that corresponding to a certain weight of delivery valve, there is a minimum weight of waste valve at which hydraulic ram functioned satisfactorily.

Multiple regression analysis was done for the data obtained on the minimum delivery head for the different combinations of weight and stroke length of both waste valve and delivery valve and an equation was developed which is given below:

$$H_{\min} = 6.7328 - 0.0132 W_w - 0.00171 W_s + 0.0305 D_w - 0.0367 D_s$$

Where H_{\min} = the minimum delivery head at which ram operates, W_w = the weight of waste valve, W_s = the stroke length of waste valve, D_w = the weight of the delivery valve, D_s = the stroke length of delivery valve. The regression analysis showed that the minimum delivery head at which ram operates has a significant influence on weight of both waste valve and delivery valve and the stroke length of the delivery valve but not the stroke length of the waste valve.

For the data presented on the delivery discharge for the different combinations of weight and stroke length of both waste valve and delivery valve and delivery discharge, a multiple regression analysis was done and an equation was developed.

$$Q_d = 5.844 - 0.3894 H_d + 0.00315 W_w - 0.004423 W_s + 0.00454 D_w - 0.00315 D_s$$

Where Q_d = delivery discharge, H_d = delivery head. From the regression analysis, it was observed that all the independent variables except stroke length of both waste valve and delivery valve were found to have significant influence on delivery discharge. This indicates that weight of waste valve has significant influence both on the delivery discharge and smooth operation of hydraulic ram. It also specifies that even though the delivery discharge corresponding to a given delivery head increases with decrease in stroke length of waste valve,

that increase is not significant. The equation indicates that discharge of hydraulic ram increases with increase in weight of both waste valve and delivery valve, whereas it decreases with increase of stroke length of both waste valve and delivery valve. The curves showing the predicted versus observed values for the minimum delivery head and delivery discharge is shown in fig. 5 and fig. 6 respectively.

Conclusions

From the study, it may be concluded that with increase in delivery head there is substantial decrease in delivery discharge. The efficiency of the hydraulic ram was found to increase with decrease in stroke length of waste valve and weight of waste valve has significant effect on delivery discharge, the smooth operation and operating range of hydraulic ram.

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